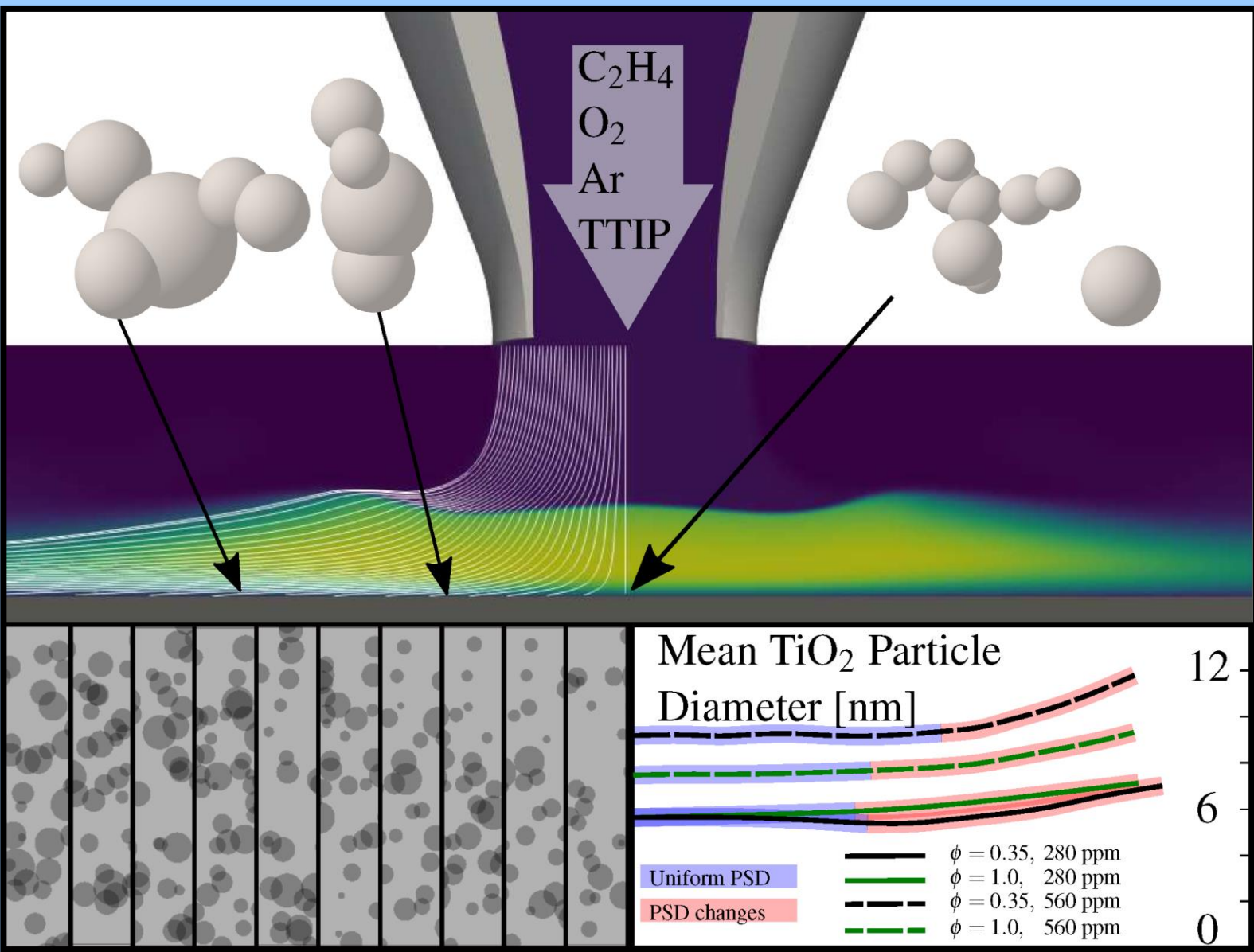


Radial dependence of TiO₂ nanoparticles synthesised in jet-wall stagnation flames

Eric J Bringley, Manoel Y Manuputty, Casper Lindberg, Gustavo Leon, Jethro Akroyd, Markus Kraft

June 25th, 2021

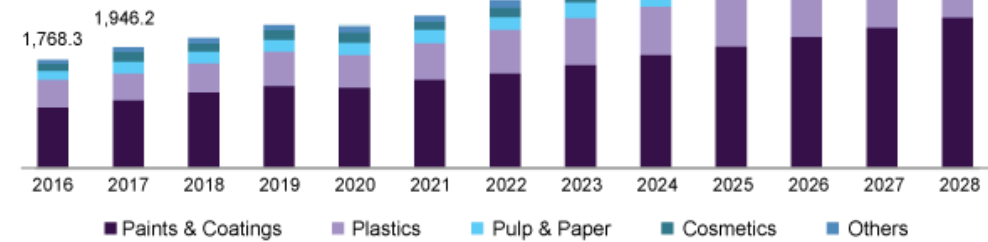


Titania (TiO₂)



U.S. TiO₂ market size, by application, 2016 - 2028 (USD Million)

\$16B Global Market

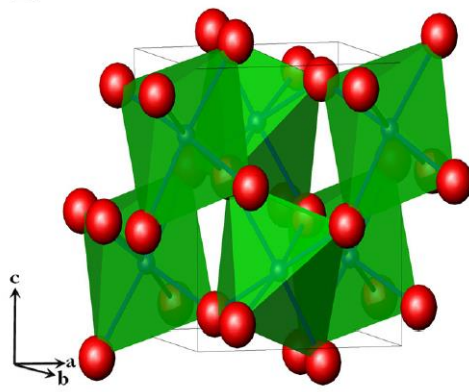
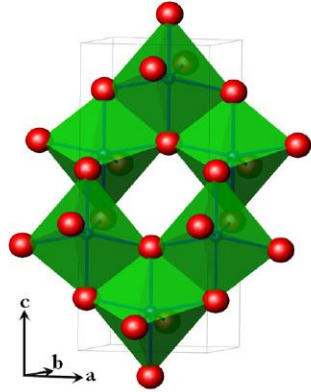
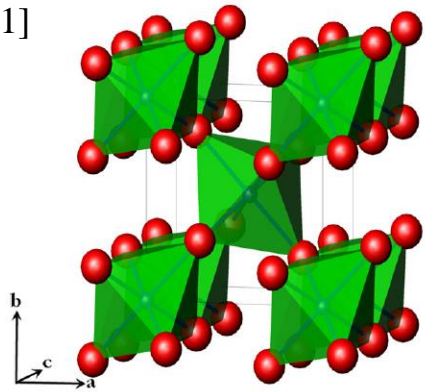


Source: www.grandviewresearch.com

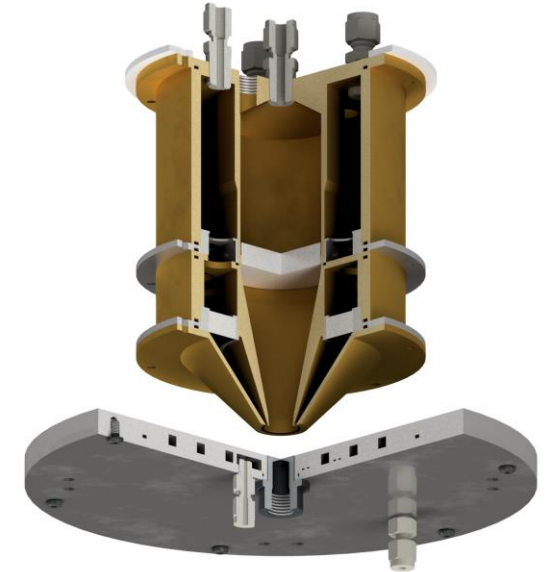
Stable Phases (Anatase, Rutile)

Metastable Phases (TiO₂-II)

[1]



[2]



[1] Aravindan et. al (2015) [doi: 10.1016/j.mattod.2015.02.015](https://doi.org/10.1016/j.mattod.2015.02.015)

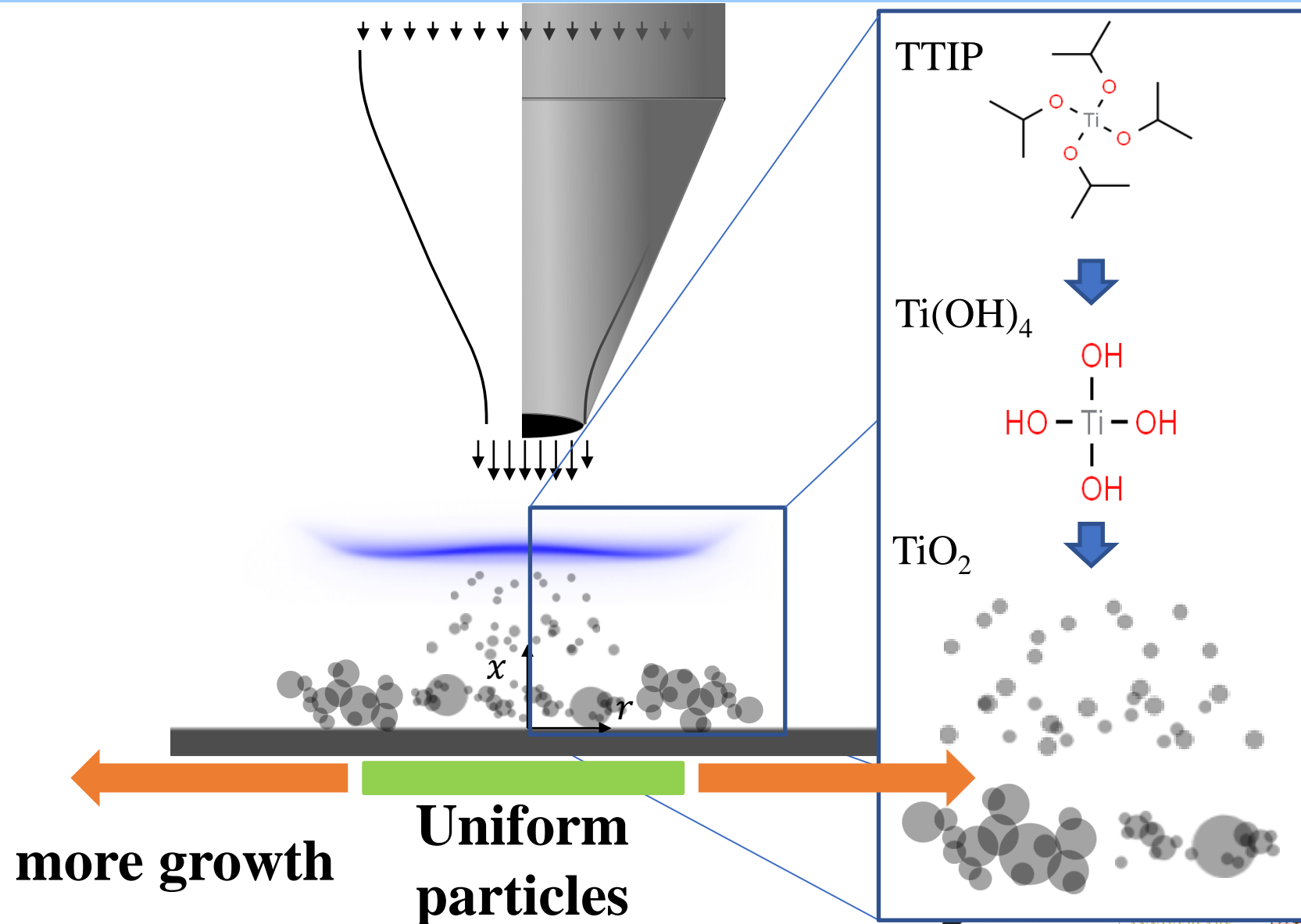
[2] Wu et. al (2020) [doi: 10.1002/smt.202000928](https://doi.org/10.1002/smt.202000928)

Jet-wall stagnation flames for TiO_2 synthesis

Short residence times
produce small particles

Do the deposited
particles change as a
function of the radius?
If so, where?

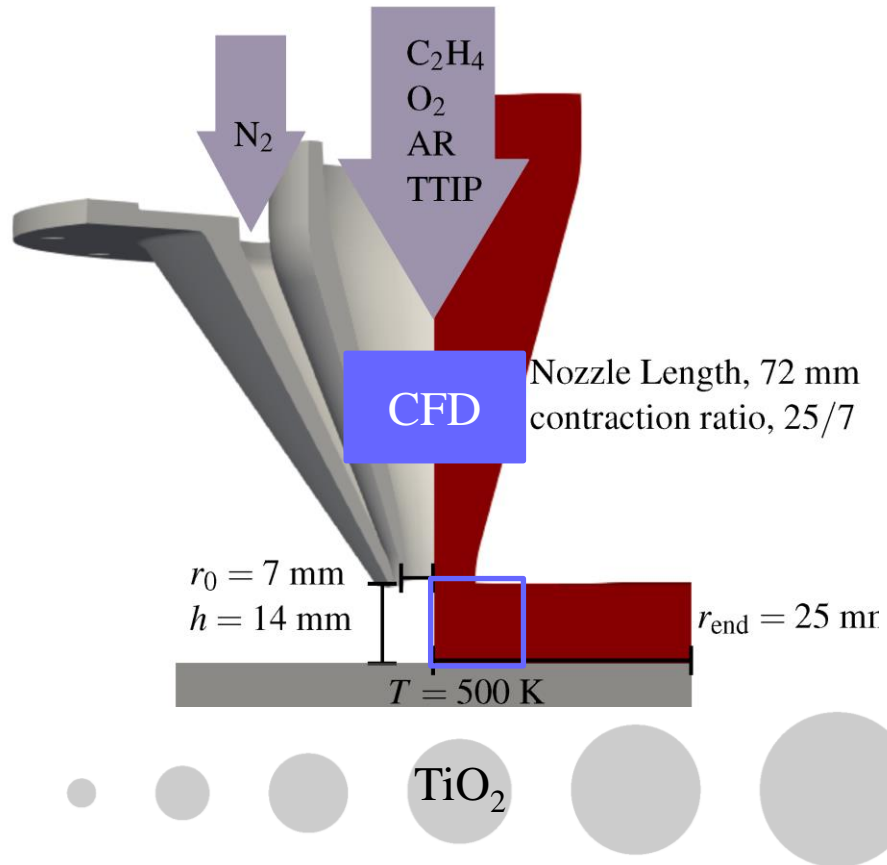
$\approx 1 - 1.5$ nozzle radius



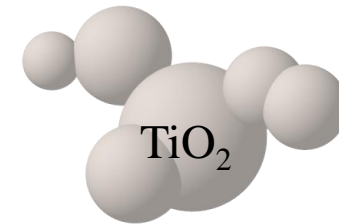
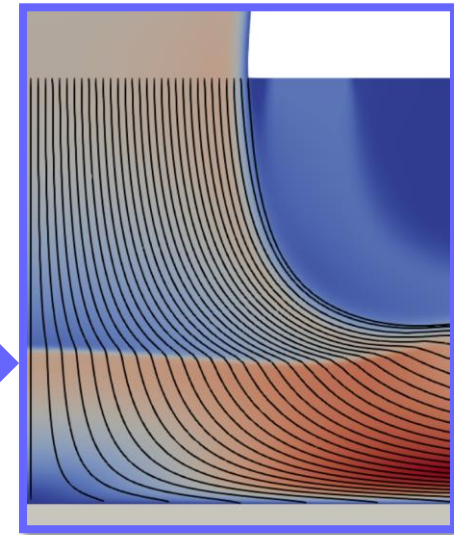
Simulations

Equivalence ratios
 $\phi = 1.0$ and 0.35

TTIP loadings
 280 and 560 ppm

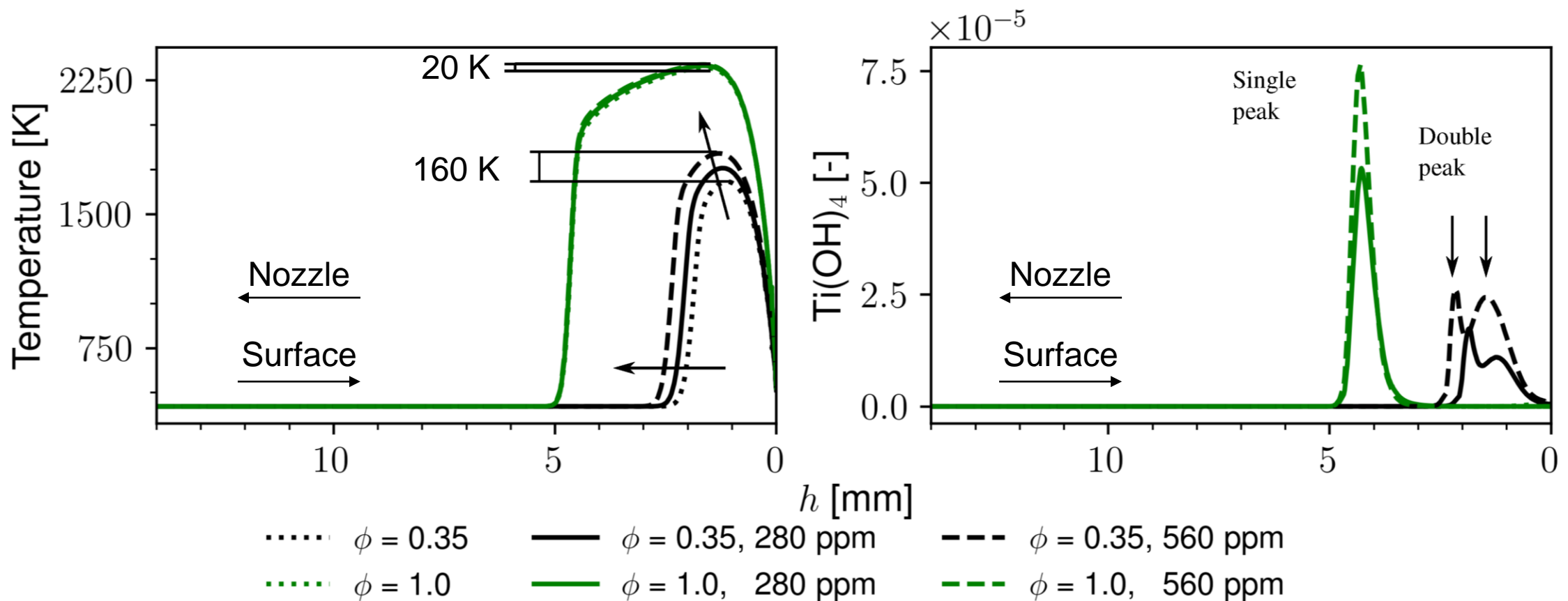


Post-process Trajectories



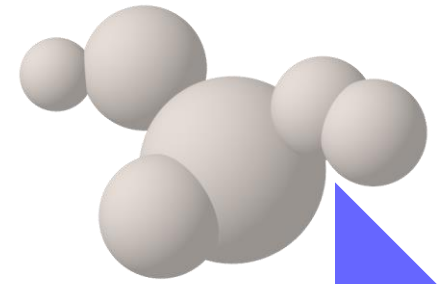
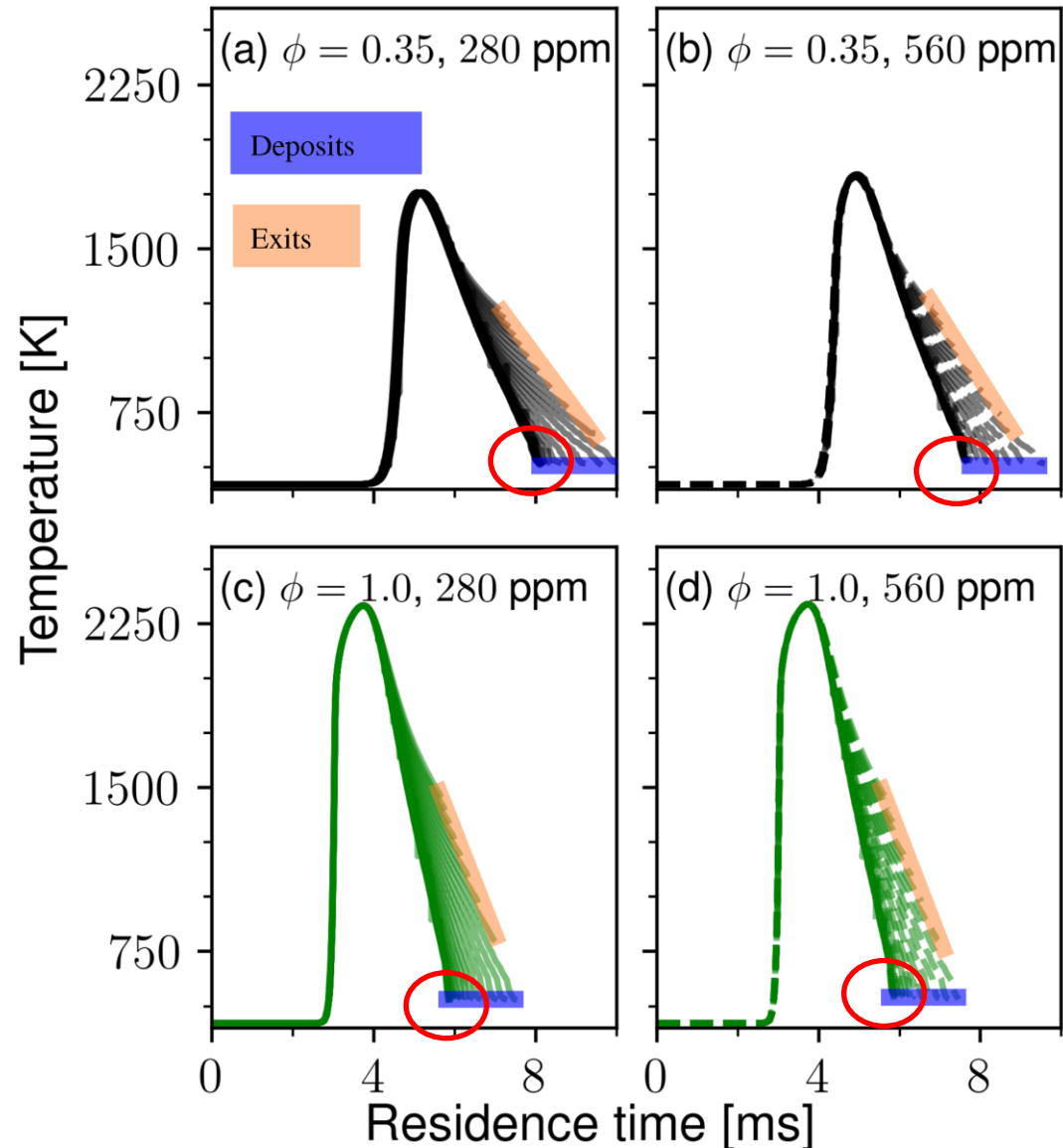
Flame centreline data

Two equivalence ratios produce different $\text{Ti}(\text{OH})_4$ profiles



Lagrangian trajectories

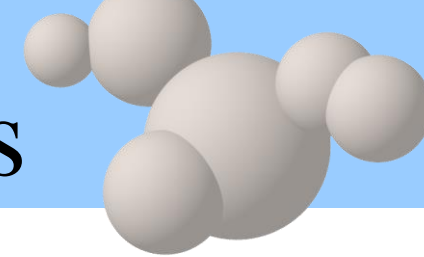
As trajectories travel further, the residence time increases.



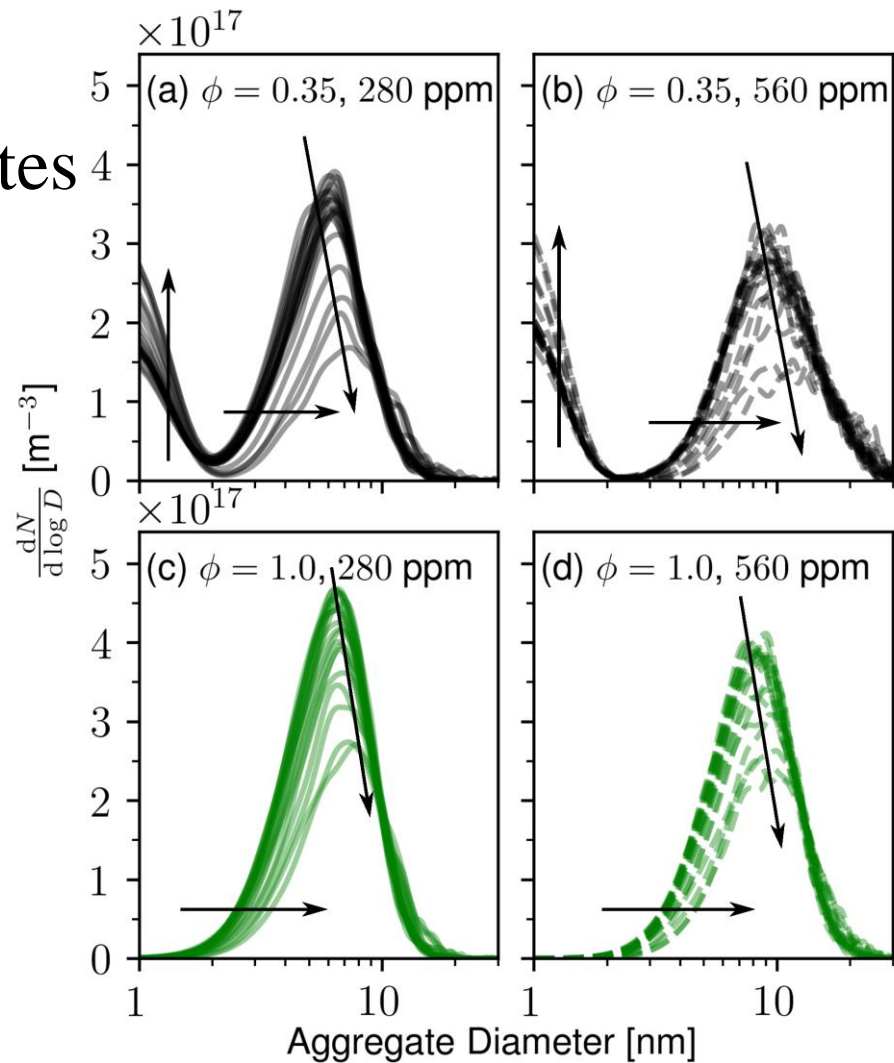
Post-processed with
Detailed Particle
Model

Aggregate and primary size distributions

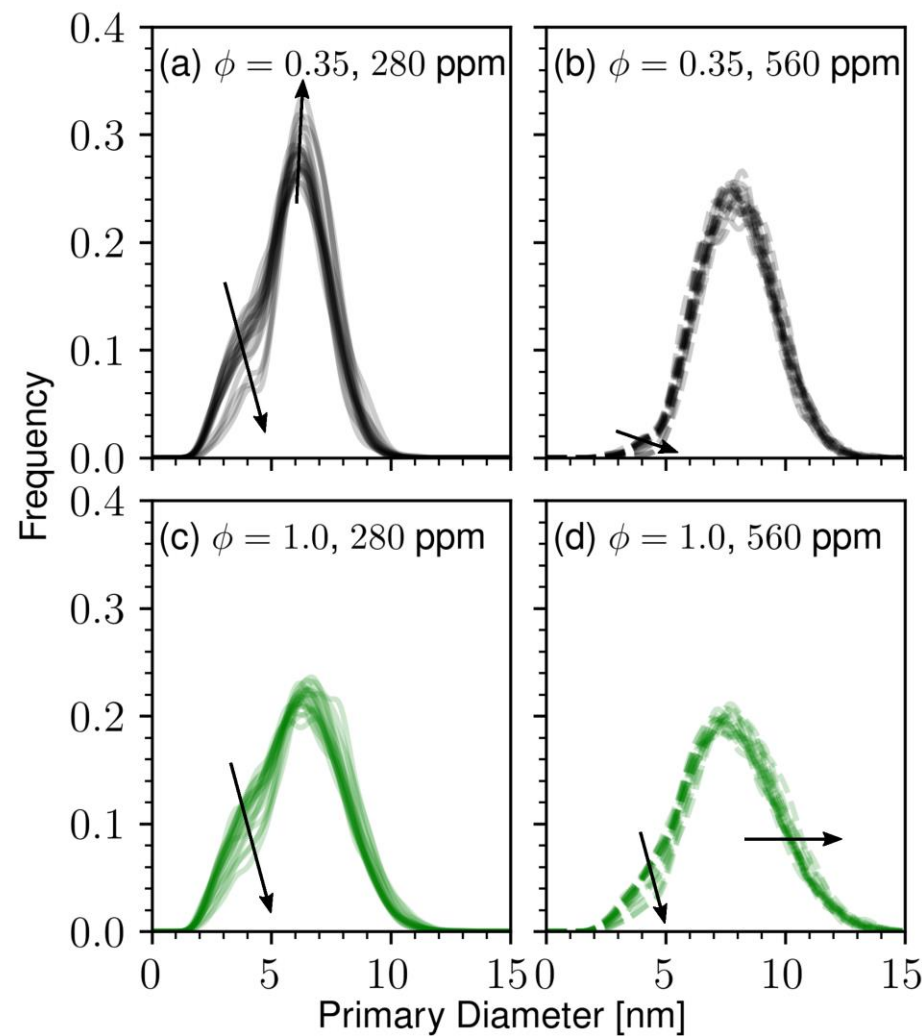
As trajectories move radially outwards,
the aggregates grow bigger, but primaries remain similar in size



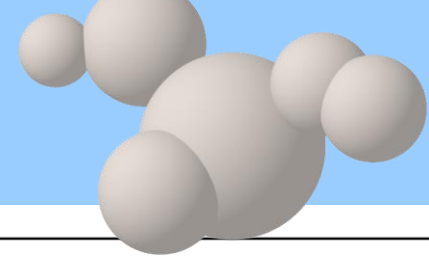
Aggregates



Primaries



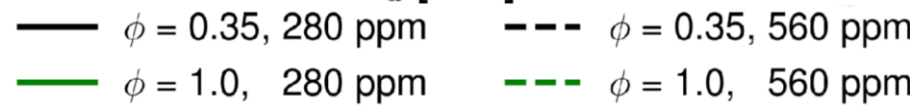
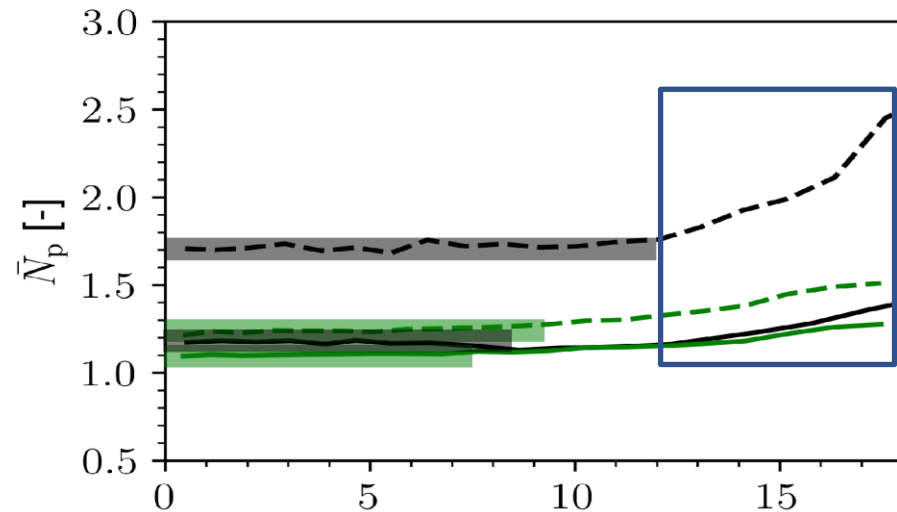
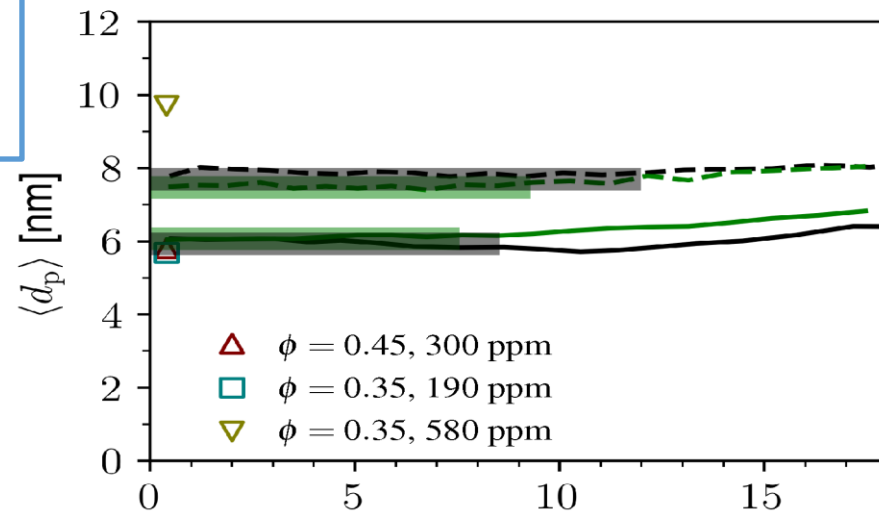
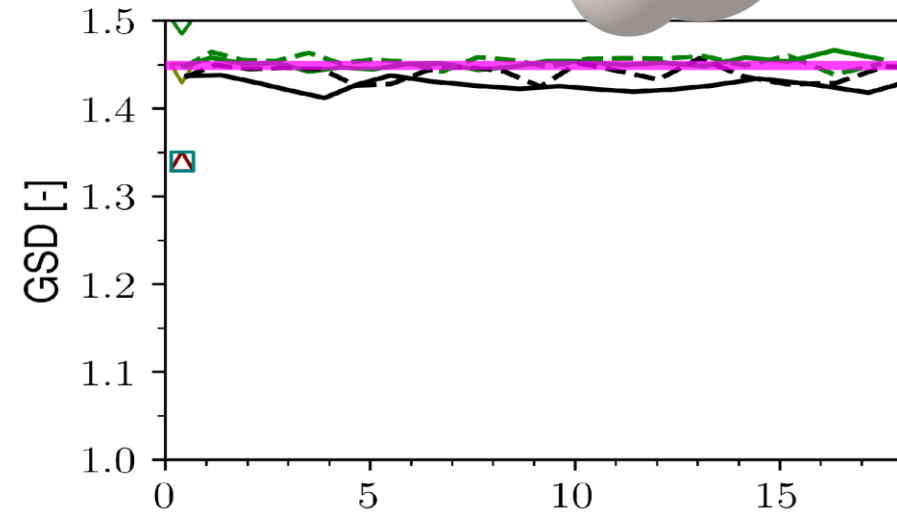
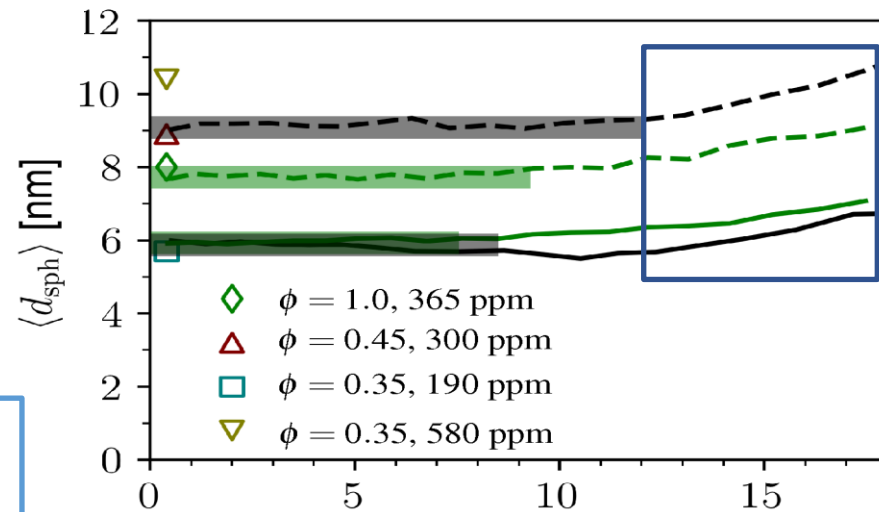
Function of deposition radius



Aggregates

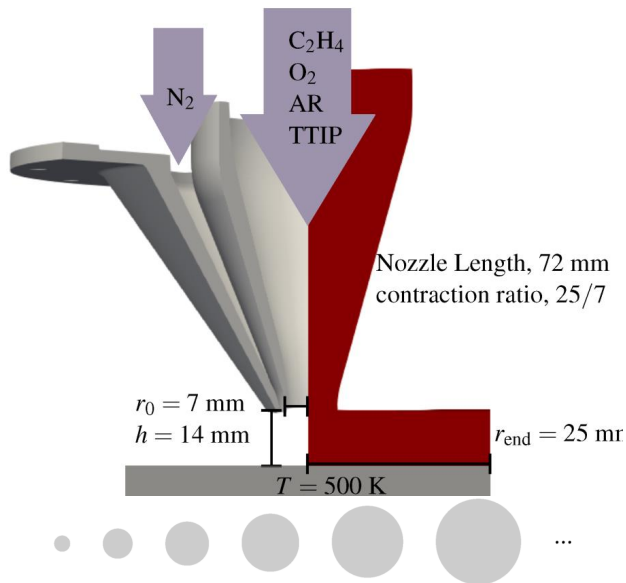
Changes to PSD are driven by more coagulation

Primaries

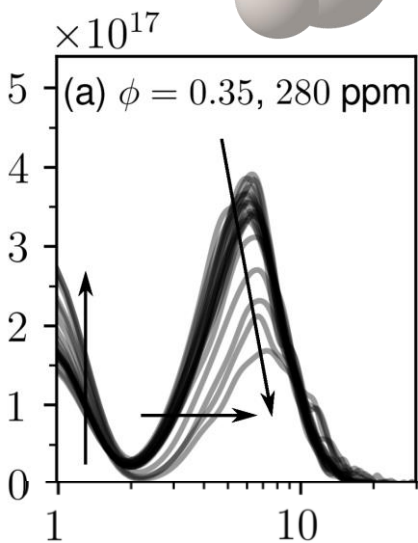
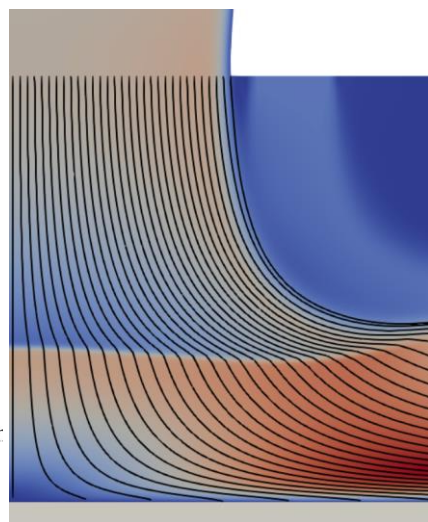


Contributions

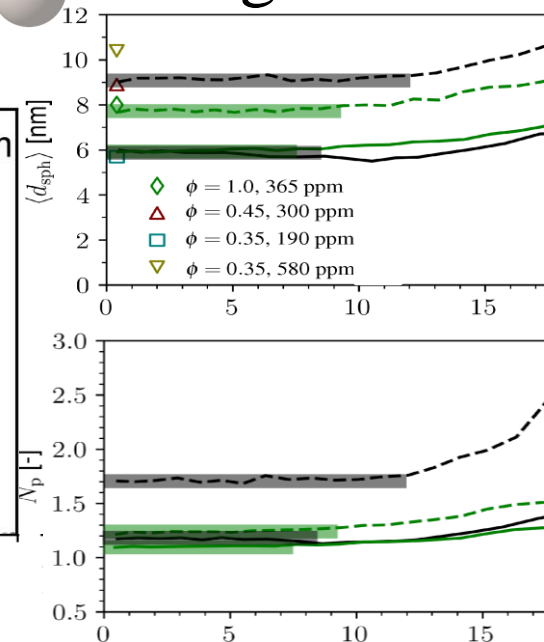
Four flames
simulated in 2D



Detailed Particle
model provided
insight into PSD



PSD differed at ≈ 1.5
nozzle radius due to
coagulation



Check performance of synthesized
particles is radially uniform

Group



Preprint



CoMo
GROUP



Team



Eric Bringley



Manoel Manuputty



Casper Lindberg



Gustavo Leon



Jethro Akroyd



Markus Kraft

CFD Equations

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho U) = 0;$$

$$\frac{\partial \rho U}{\partial t} + \nabla \cdot (\rho U U) = -\nabla p - \mu (\nabla U + (\nabla U)^T);$$

$$\frac{\partial \rho Y_i}{\partial t} + \nabla \cdot (\rho U Y_i) + \nabla \cdot (\rho V_i^c Y_i) = \dot{\omega}_i;$$

$$c_p \frac{\partial \rho T}{\partial t} + c_p \nabla \cdot (\rho U T) = \nabla \cdot (\lambda \nabla T) - \left(\rho \sum_{i=1}^N c_{p_i} Y_i V_i^c \right) \cdot \nabla T + \dot{\omega}_T$$

$$\frac{\partial \rho \hat{M}_j}{\partial t} + \nabla \cdot (\rho U \hat{M}_j) + \nabla \cdot (\rho V_T \hat{M}_j) = \nabla \cdot \left(\rho D_{p1} \nabla \hat{M}_{j-\frac{2}{3}} \right) + \dot{\omega}_j$$



Closure Models

Viscosity

$$\mu = \sum_{i=1}^N \frac{X_i \mu_i}{\sum_{j=1}^N X_j \phi_{ij}}$$

$$\phi_{ij} = \frac{1}{\sqrt{8}} \left(1 + \frac{W_i}{W_j}\right)^{-\frac{1}{2}} \left(1 + \left(\frac{\mu_i}{\mu_j}\right)^{\frac{1}{2}} \left(\frac{W_j}{W_i}\right)^{\frac{1}{4}}\right)^2$$

Thermal Conductivity

$$\lambda = \frac{1}{2} \left(\sum_{i=1}^N X_i \lambda_i + \left[\sum_{i=1}^N X_i / \lambda_i \right]^{-1} \right)$$

Diffusion

Binary $D_{i,j} = \frac{3}{16} \left(\frac{2N_A k_B^3 T^3}{\pi W_{ij}} \right)^{1/2} \frac{1}{p \sigma_{ij}^2 \Omega^{(1,1*)}}$

Mixture-Averaged: $D_i = \frac{1 - Y_i}{\sum_{j \neq i}^N \frac{X_j}{D_{ij}}}$

Diffusion Velocity: $V_i = -D_i \frac{\nabla X_i}{X_i}, \quad V_c = -\sum_j^N Y_j V_j$

Corrected Diffusion Velocity: $V_i^c = V_i + V_c$

Closure Models

Thermodynamic Properties, JANAF Polynomials

$$c_{p_i} = \frac{C_{p_i}}{W_i} = \frac{R_g}{W_i} (a_{1,i} + a_{2,i}T + a_{3,i}T^2 + a_{4,i}T^3 + a_{5,i}T^4) \quad c_p = \sum_{i=1}^{N_{sp}} Y_i c_{p_i}$$

$$h_i = \frac{H_i}{W_i} = \frac{R_g}{W_i} \left(a_{1,i}T + \frac{a_{2,i}}{2}T^2 + \frac{a_{3,i}}{3}T^3 + \frac{a_{4,i}}{4}T^4 + \frac{a_{5,i}}{5}T^5 + a_{6,i} \right) \quad h = \sum_{i=1}^{N_{sp}} Y_i h_i$$

Ideal Gas Law

$$pV = nRT$$

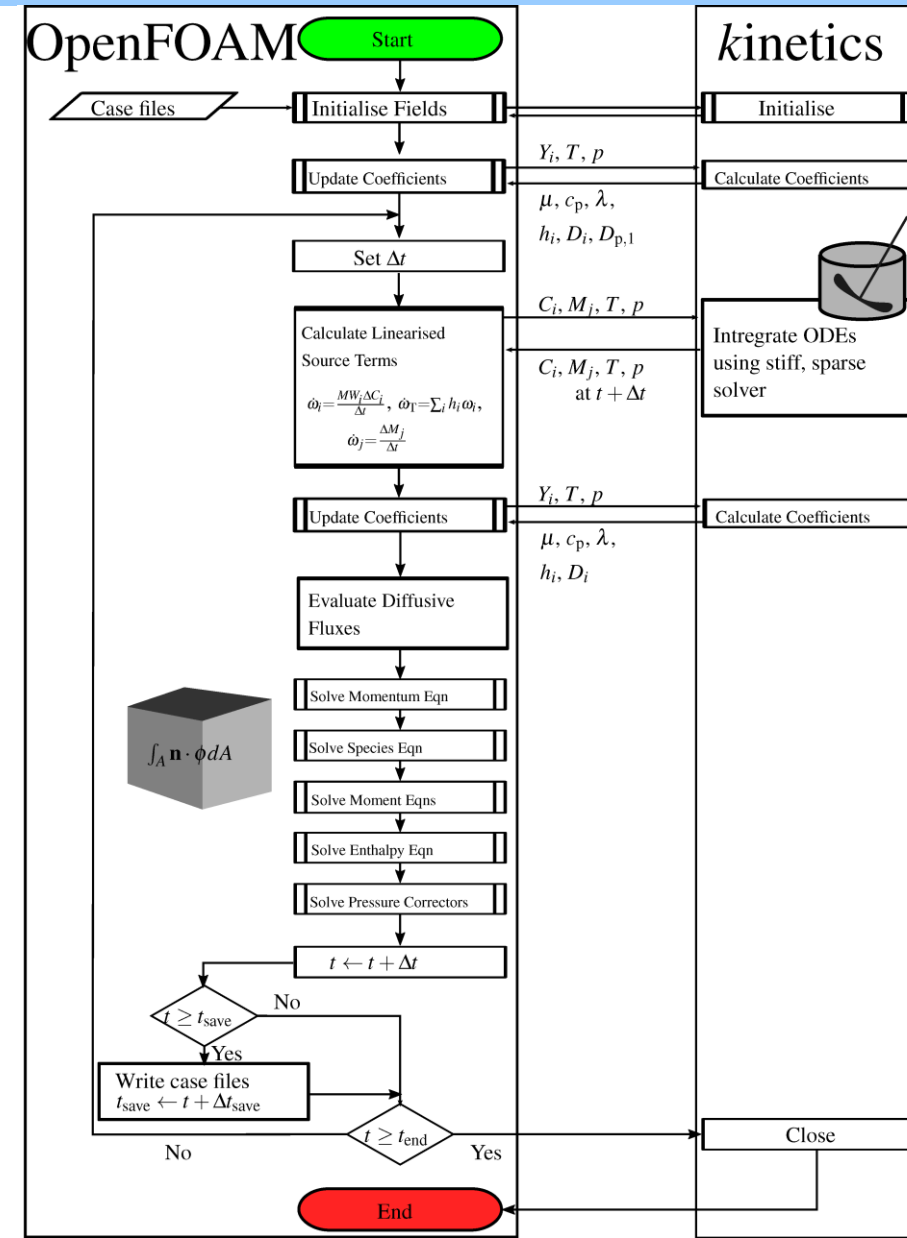
Models and methods: flow

2D Simulations:

Navier Stokes Equations,
CFD with PISO Alg.

CFD Models:

Ideal Gas Law, JANAF,
Mixture Avg. Transport,
UCSD Chemistry



Models and methods: TiO₂ particles

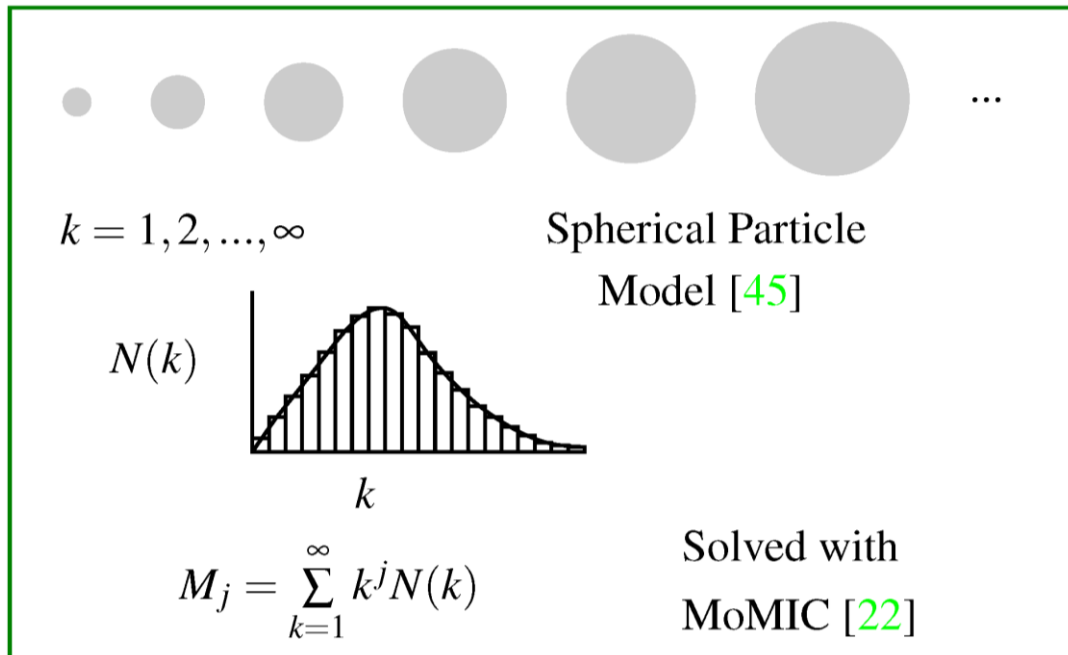
Computational efficiency

vs

Physical insight

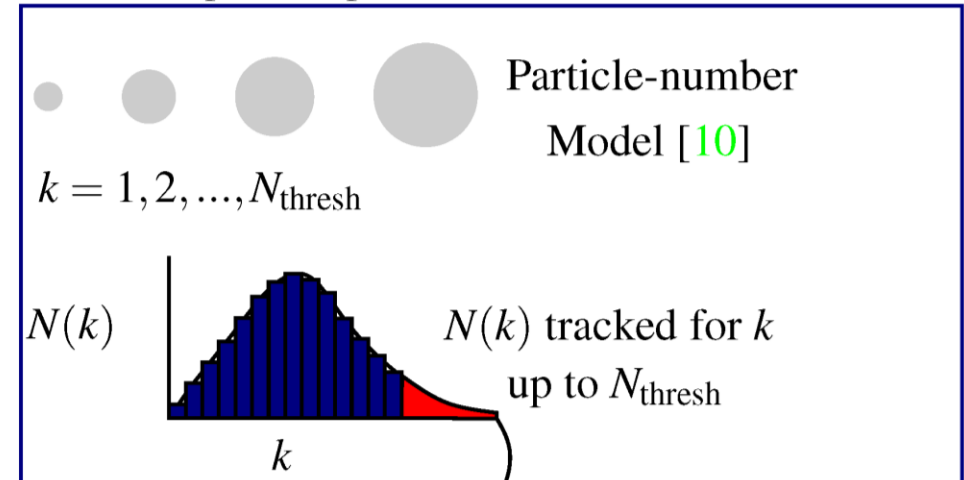
Same gas phase transfer species, Ti(OH)₄
Particle inception, surface growth, and coagulation

Coupled to governing equations

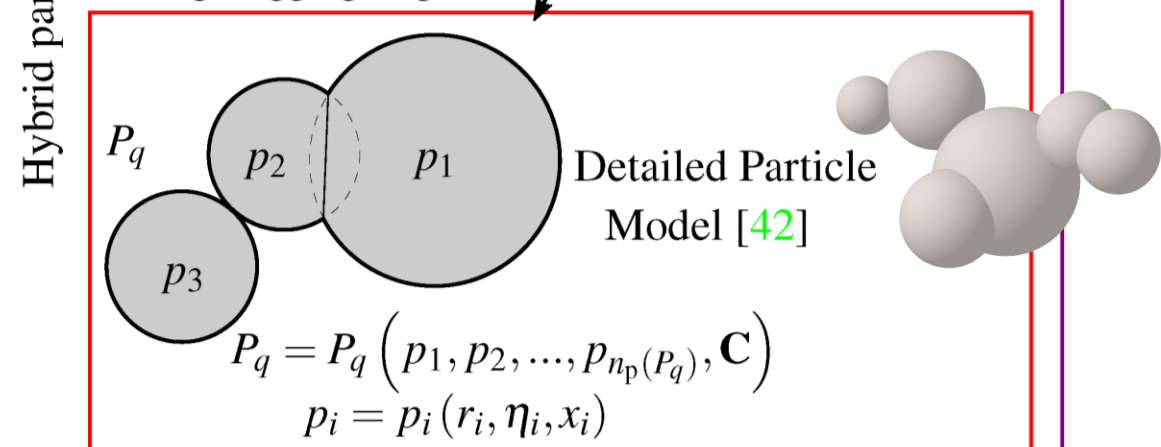


Lagrangian post-processing

for small, spherical particles:



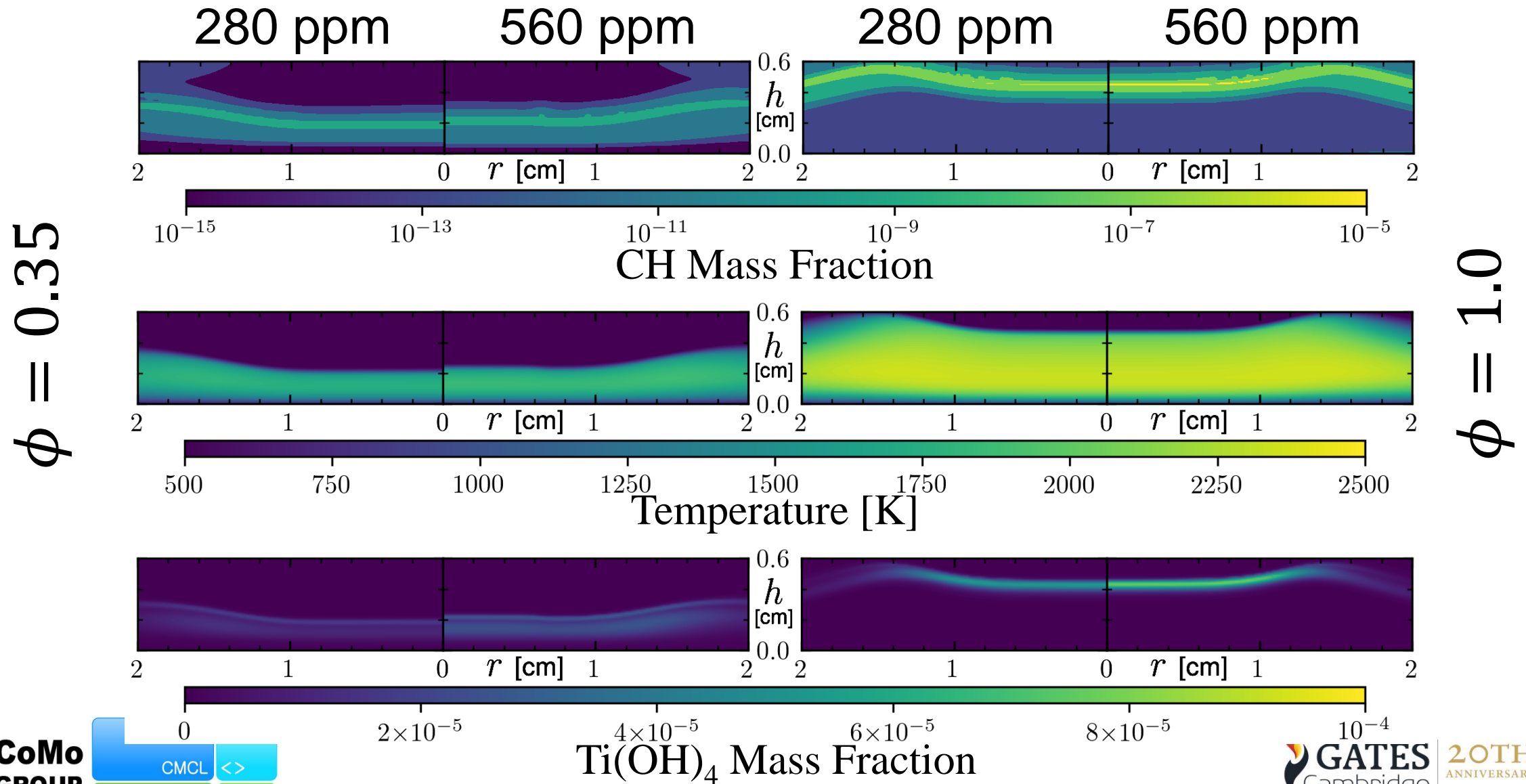
for large, aggregate particles:



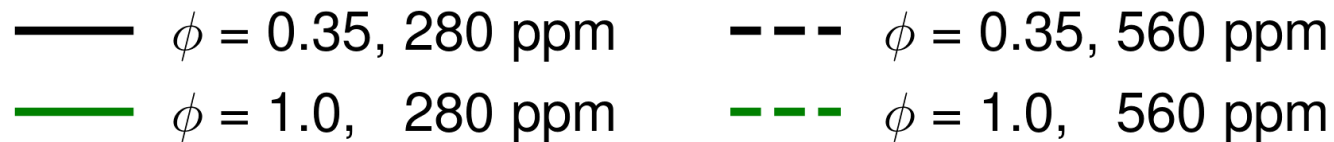
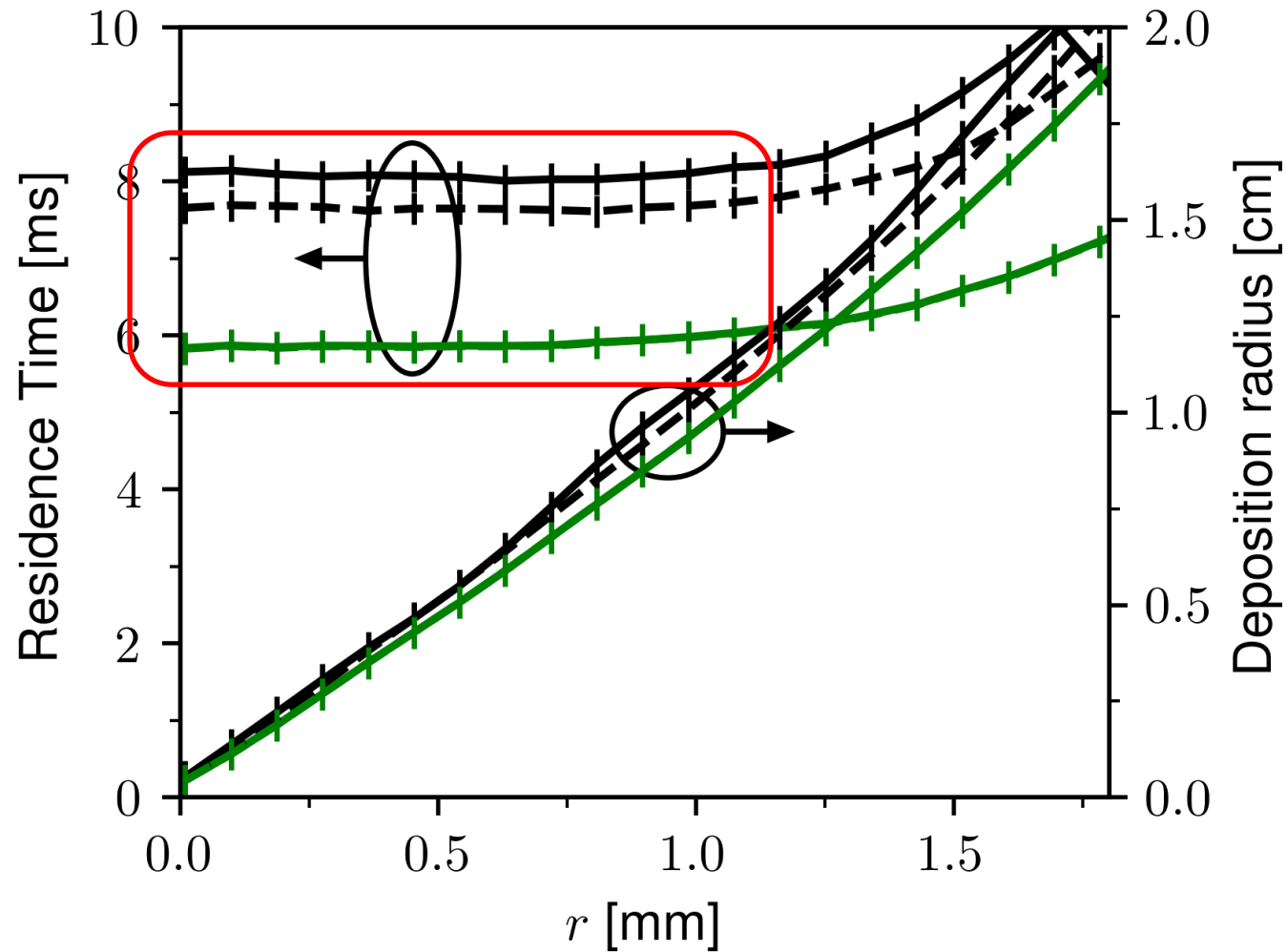
Solved with a DSMC method [18]

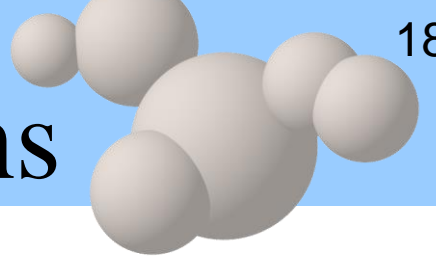


Flame data



Trajectory properties



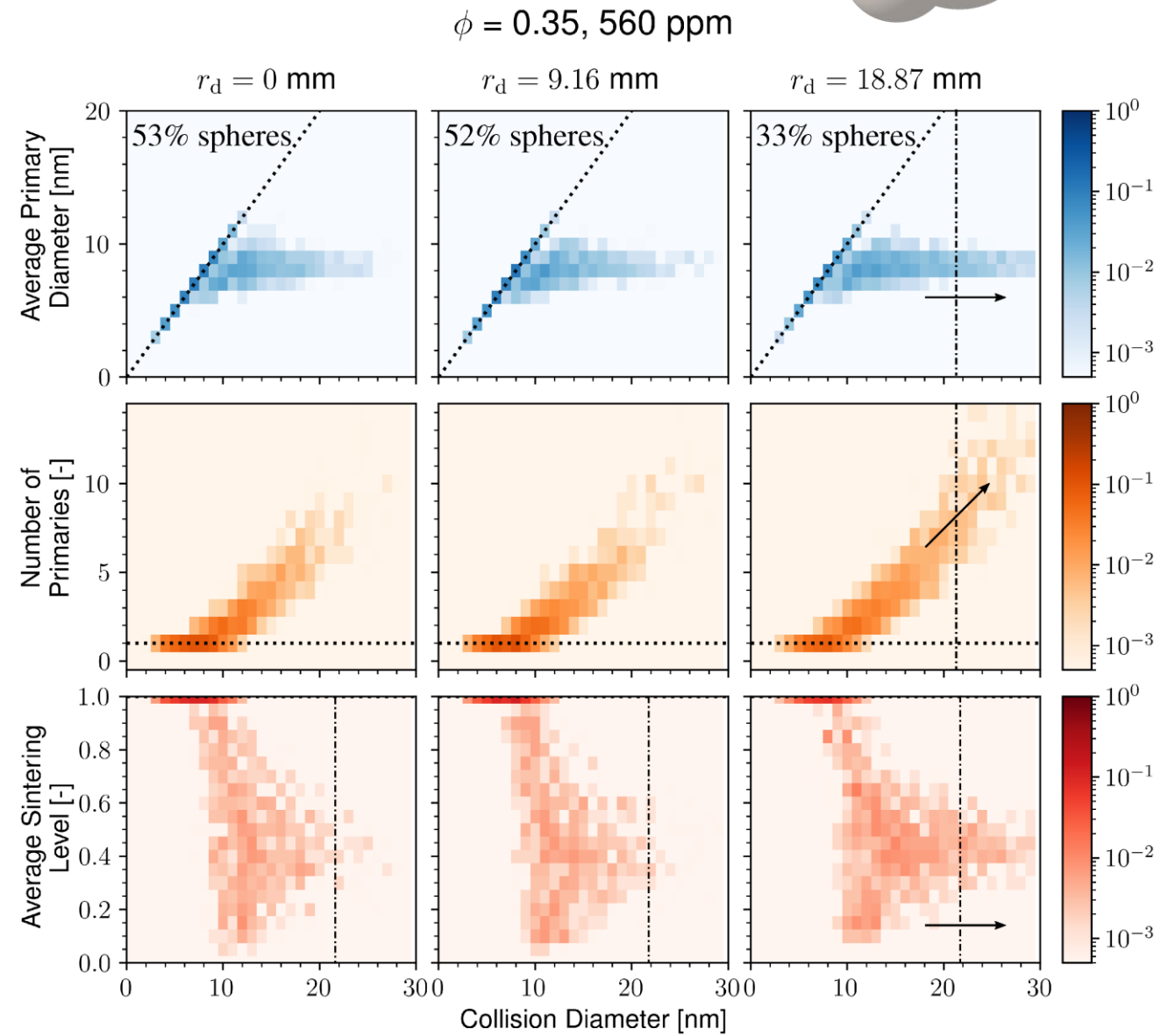


Primaries particle joint property distributions

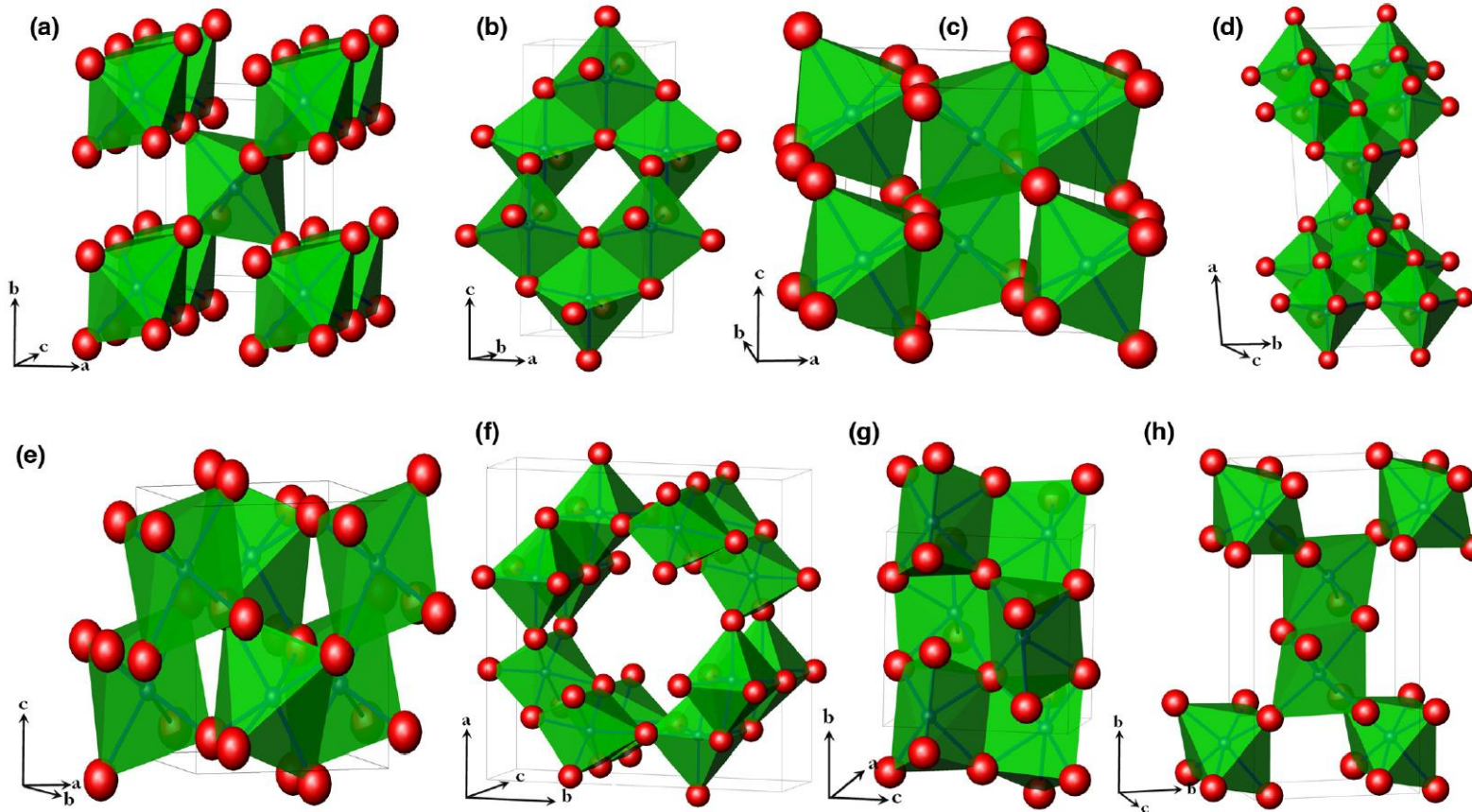
Average primary diameter does not significantly change

Large particles at large radius have a high number of primaries

Large particles are weakly sintered



Titania crystal phases



- (a) Rutile
- (b) Anatase
- (c) Bronze
- (d) Brookite
- (e) Columbite
- (f) Hollandite
- (g) Baddeleyite
- (h) Ramsdellite

Figure from Aravindan et. al (2015),
<https://doi.org/10.1016/j.mattod.2015.02.015>